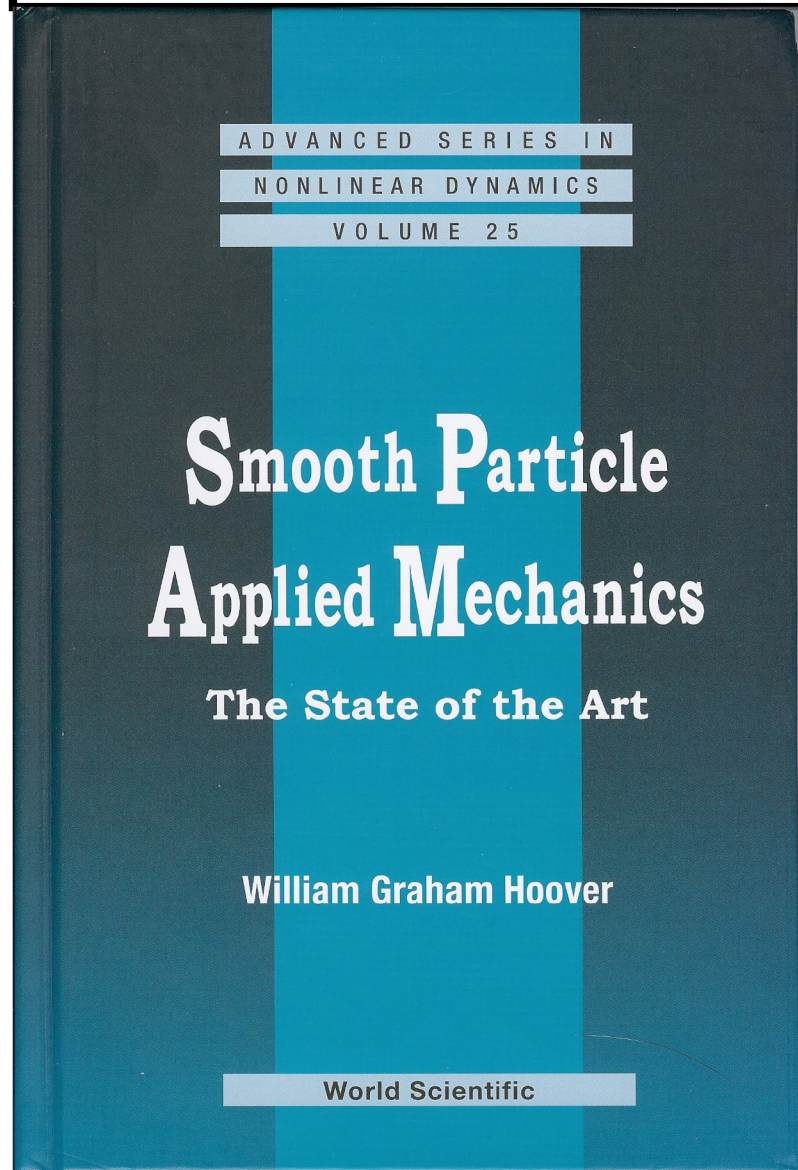


# Smooth Particle Applied Mechanics



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**Lectures presented in  
Mexico City, Mexico  
January 2007**

# **SPAM: A Novel and Simple Method for Solving the Continuum Equations**

## **➤ SPAM Theory**

- 1. Continuum Mechanics (PDEs)**
- 2. Numerical Solution Methods**
  - a) Finite Element Method**
  - b) Particle Method (Motivation)**
- 3. SPAM Interpolation & Gradients**
- 4. SPAM ODEs**
- 5. Runge-Kutta Time Integration**
- 6. Molecular Dynamics Analogs**
- 7. Mesh Generation & Boundary Conditions**
- 8. Maladies and Cures**

## **➤ SPAM Results**

- 9. Free Expansion**
- 10. Parallel Techniques**
- 11. Collapsing Fluid Column**
- 12. Rayleigh-Bénard Flow**
- 13. Research problems**
  - a) Tension Test**
  - b) Ball Plate Problem**

# 1. Continuum Theory : Microscopic *versus* Macroscopic Material Descriptions

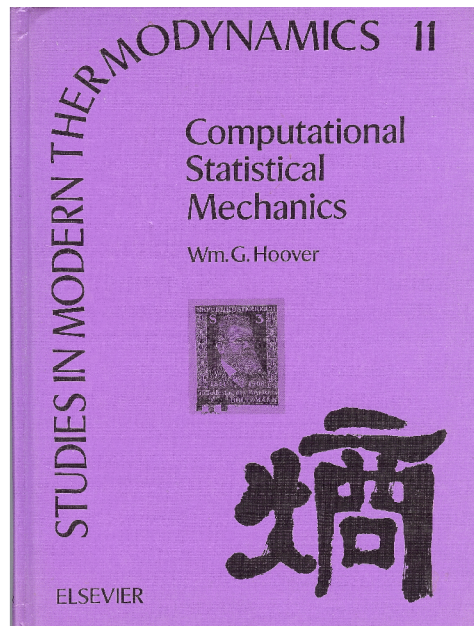
## Microscopic Description

Atomistic length & time scales

$L \sim \text{\AA}$   
 $t \sim \text{ps-ms}$  (vibrational frequencies)

Follow atomic motion with  
**ordinary differential equations**

Specify force laws for atoms



## Macroscopic Description

Laboratory length & time scales

$L \sim \text{cm or meters}$   
 $t \sim \text{ms or seconds}$

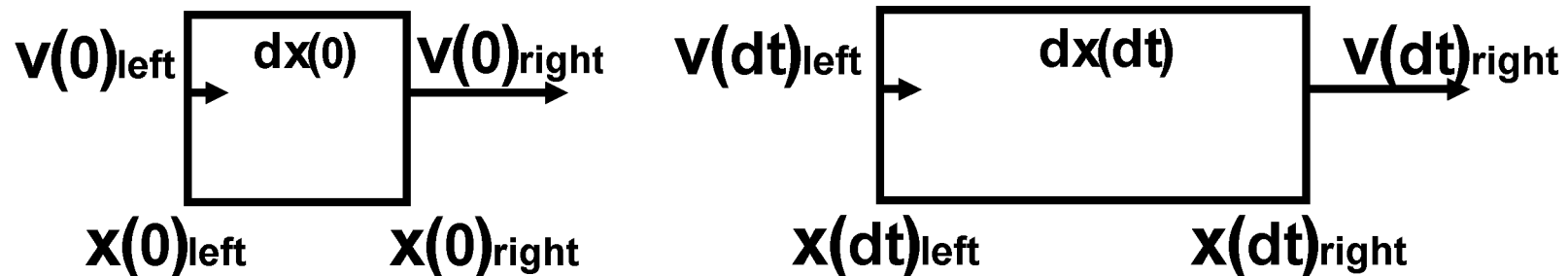
Material flow or solid deformation satisfy **partial differential equations**

Specify constitutive relations for the materials

← **For a pdf file, go to [www.williamhoover.info](http://www.williamhoover.info)**

# 1. Continuum Theory: Continuity Equation - Conservation Law for Mass

Lagrangian description follows the motion of material points:



$$x_{\text{right}} \rightarrow x_{\text{right}} + v dt + \frac{dx}{2} (\partial v / \partial x)_t dt$$

$$x_{\text{left}} \rightarrow x_{\text{left}} + v dt - \frac{dx}{2} (\partial v / \partial x)_t dt$$

$$dx(0) \rightarrow dx(0) [1 + (\partial v / \partial x)_t dt] = dx(dt)$$

$$\frac{dx(dt) - dx(0)}{dt dx(0)} \rightarrow \frac{d(\ln dx)}{dt} \equiv - \frac{d \ln \rho}{dt} = \frac{\partial v}{\partial x}$$



# 1. Continuum Theory: Lagrangian Equations, Pressure, Heat Flux

$$\dot{\rho} = -\rho \nabla \cdot \mathbf{v}$$

$$\rho \dot{\mathbf{v}} = -\nabla \cdot \mathbf{P}$$

$$\rho \dot{e} = -\nabla \mathbf{v} : \mathbf{P} - \nabla \cdot \mathbf{Q}$$

with

$$\mathbf{P} = \mathbf{P}(\rho, e, ?) ; \mathbf{Q} = \mathbf{Q}(\rho, e, ?) .$$

# 1. Continuum Theory

## Equilibrium Fluid Constitutive Equations

Mechanical equation of state (adiabatic and isothermal):

$$P = B_o \left( \frac{\rho^3}{\rho_o^3} - \frac{\rho^2}{\rho_o^2} \right)$$

Thermal equation of state and Mechanical equation of state:

$$E = NDkT/2; PV = NkT = \frac{2}{D}E$$

Heat capacity and compressibility:

$$dE/dT_{V \text{ or } P} > 0; -1/V(\partial V/\partial P)_{T \text{ or } S} > 0$$

Van der Waals' :

$$P = \frac{NkT}{V - Nb} - \frac{N^2a}{V^2}; E = \frac{DNkT}{2} - \frac{N^2a}{V}$$

# 1. Continuum Theory

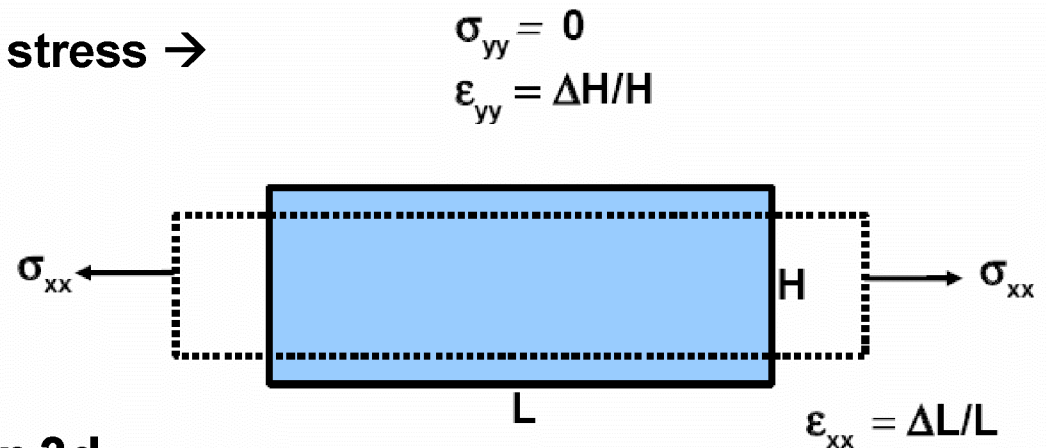
## Nonequilibrium Constitutive Relations

- Nonequilibrium dissipation: viscosity, conductivity, plasticity, ...
- Fourier's law:

$$\mathbf{Q} = -\kappa \nabla T.$$

- Newton's formulation of shear stress → symmetrized stress tensor :

$$\sigma = \sigma_{eq} \mathbf{I} + \lambda |\nabla \cdot \mathbf{v}| + \eta [\nabla \mathbf{v} + \nabla \mathbf{v}^t]$$



$$\eta_v = \eta + \lambda \text{ in 2d}; \eta_v = \frac{2}{3}\eta + \lambda \text{ in 3d}.$$

$$E = \sigma_{xx} / \epsilon_{xx} ; \nu = -\epsilon_{yy} / \epsilon_{xx}$$

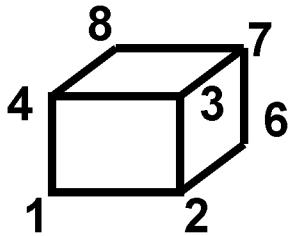
- Use von Mises shear stress condition for plasticity :

$$(\sigma_{xx}^2 - \sigma_{yy}^2)^2 + 4\sigma_{xy}^2 \leq Y^2 \text{ in 2d}.$$

## 2. a) Numerical Solution Methods Finite-Elements (DYNA3D and ParaDyn)

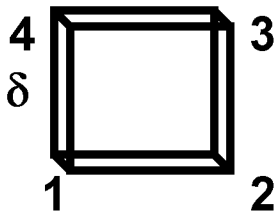
Use space-filling volumes to approximate the continuum:

- 8-Node brick has *isoparametric* velocity interpolation for strain rates:



$$\mathbf{v}(\mathbf{x}, \mathbf{y}, \mathbf{z}) = \mathbf{a}_1 + \mathbf{a}_2 \mathbf{x} + \mathbf{a}_3 \mathbf{y} + \mathbf{a}_4 \mathbf{z} \\ + \mathbf{a}_5 \mathbf{xy} + \mathbf{a}_6 \mathbf{yz} + \mathbf{a}_7 \mathbf{zx} + \mathbf{a}_8 \mathbf{xyz}$$

- 4-Node shell elements are *two-dimensional*. They have a thickness  $\delta$  and various underlying through-the-thickness integration schemes.

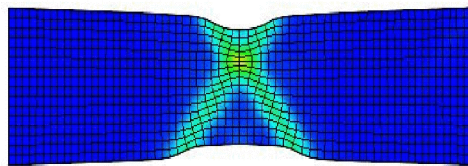
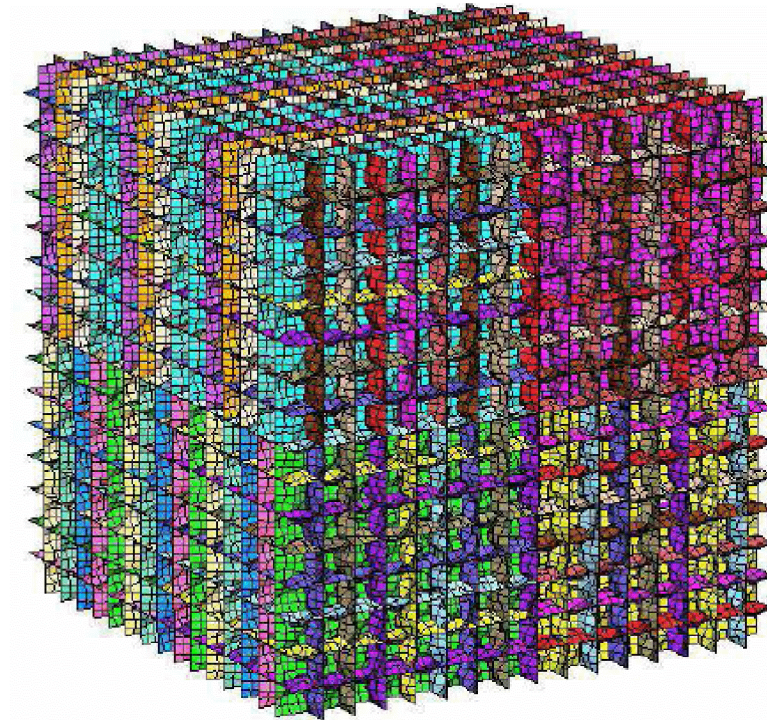
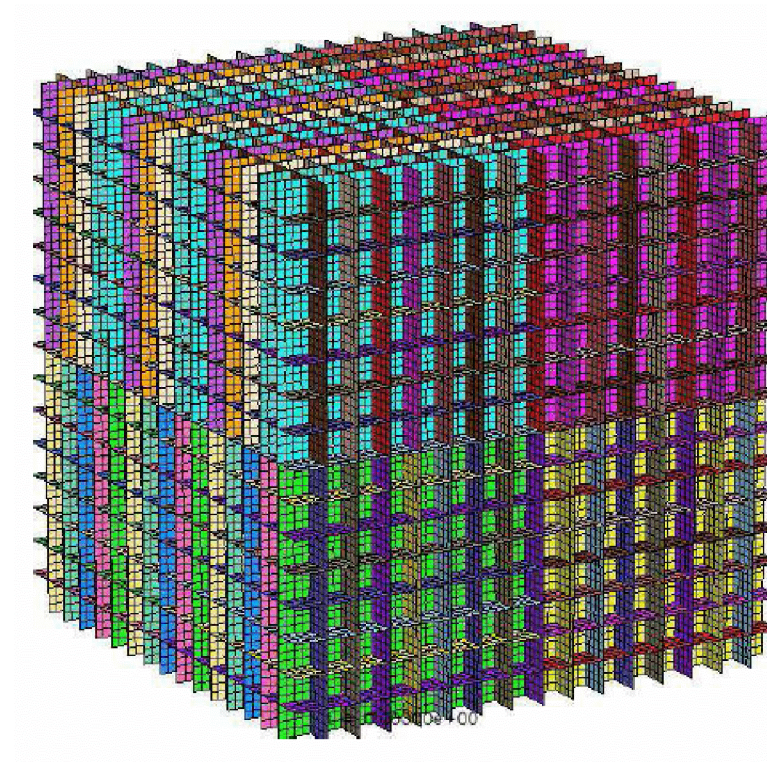


$$\mathbf{v}(\mathbf{x}, \mathbf{y}) = \mathbf{a}_1 + \mathbf{a}_2 \mathbf{x} + \mathbf{a}_3 \mathbf{y} + \mathbf{a}_4 \mathbf{xy}$$

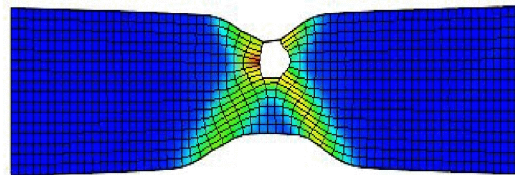
- Calculate pressure, energy, stress by integrating over elements (for example, nodal strain/strain rates, element integration → stresses)

Lin, DYNA3D, UCRL-MA-107254 & Hoover, *et alii*, ParaDyn, UCRL-MA-140943  
from Methods Development Group, Lawrence Livermore National Laboratory .

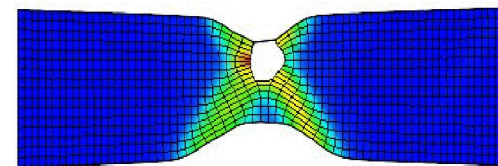
## Two Example Finite-Element Calculations



**Time = 32**



**Time = 48**



**Time = 64**



## 2. b) Numerical Solution Methods

### Particle Methods – Motivation & Example

#### History

Smooth particles used for astrophysics problems :

Gingold, Lucy, and Monaghan - 1977

Smooth particles applied to fluids and solids (~1990)

#### Motivation

Fluids and solids satisfy the **same** motion equations

No element integration

No mesh tangling for flow problems

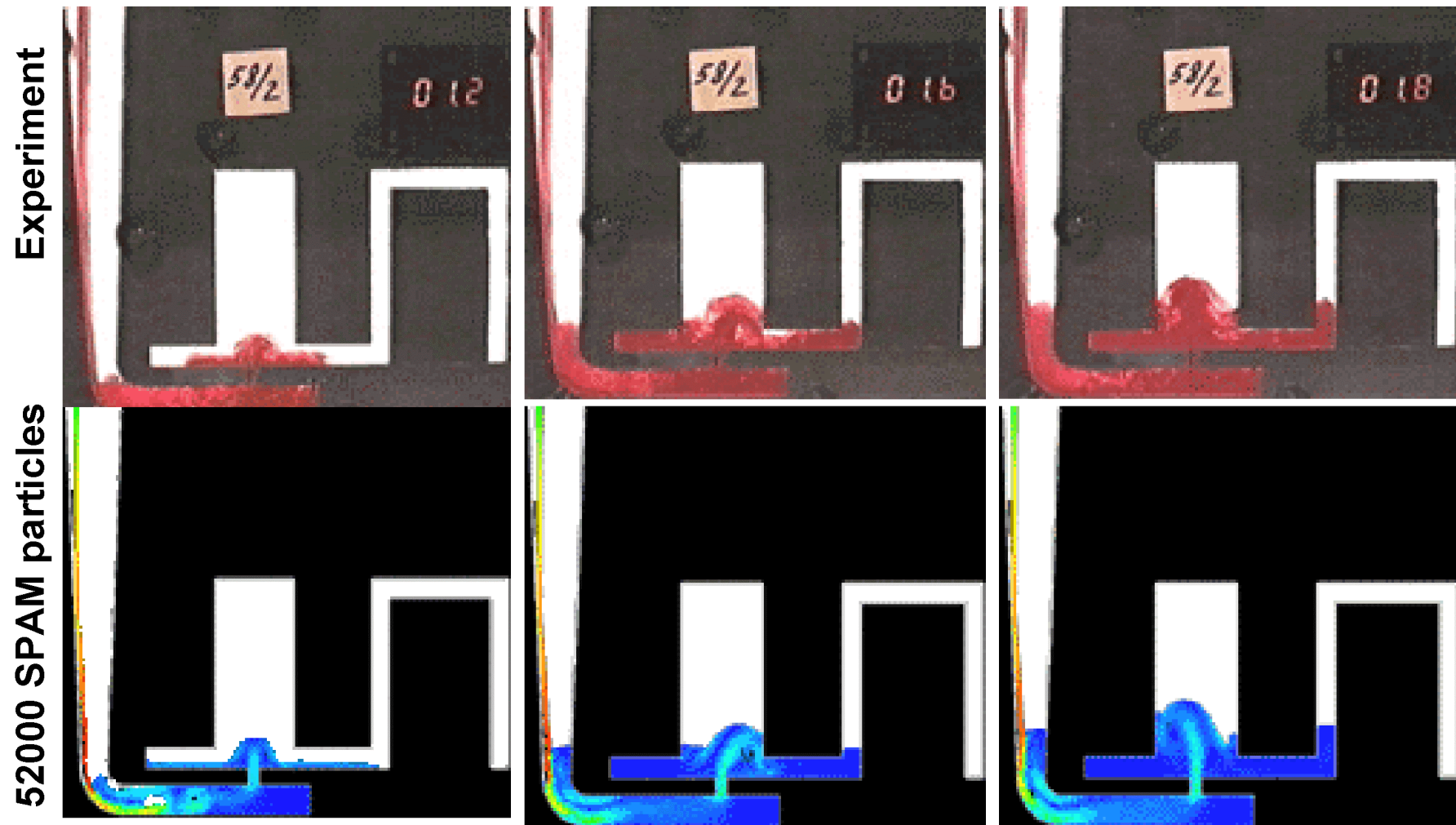
Material failure is simple with Lagrangian particles

Applications in **many** fields (heat conduction, electricity & magnetism, fluid structure interaction, fragmentation, ...)

**Simplify! Simplify! Simplify!**  
**(Thoreau)**

# High Pressure Die Casting Experiment/Simulation

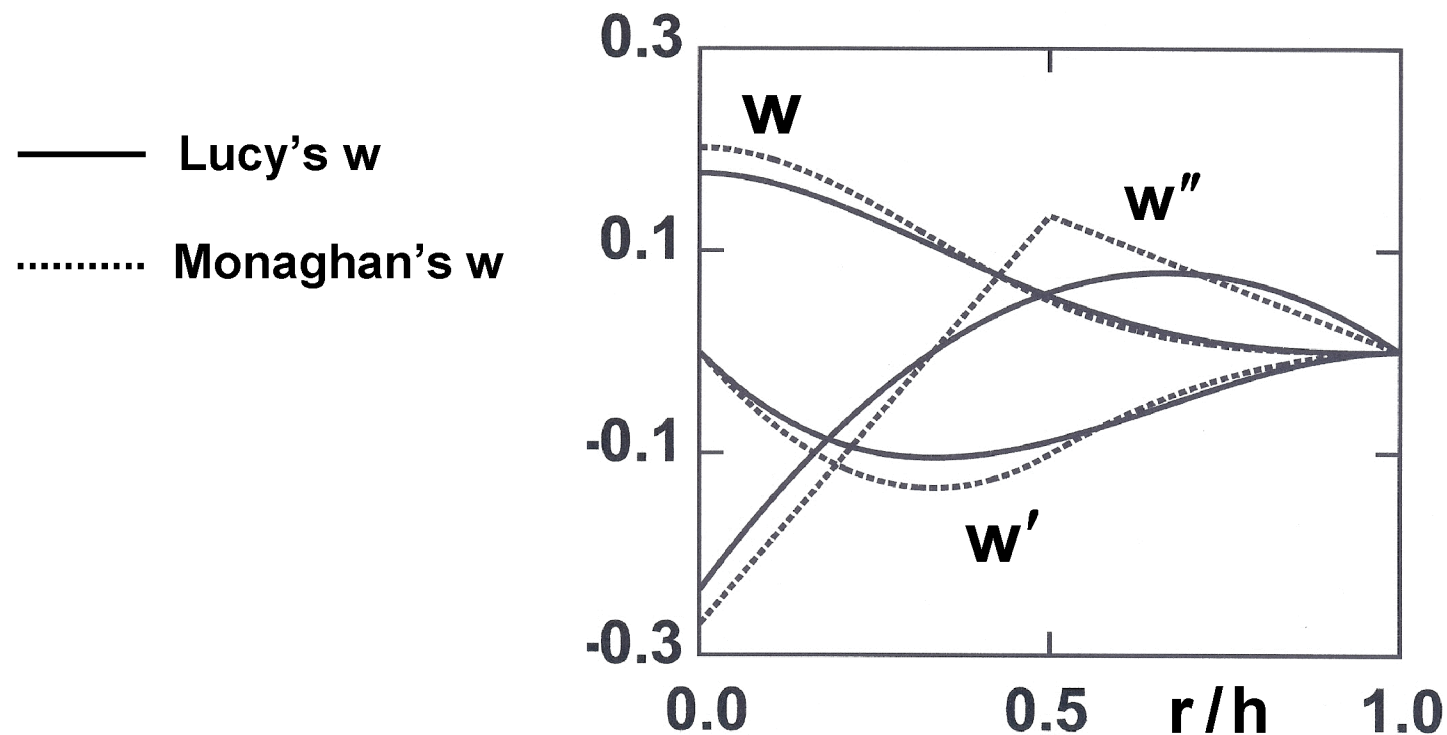
Ha, Cleary, Alguine & Nguyen@<http://www.cmis.csiro.au/cfd/sph/>



### 3. Spatial Interpolation and Gradients

Particles of Finite Extent Represent the Continuum .

Particles with an extent  $h$  represent a continuum.  
The particle **weight function**,  $w$ , as well as its first two spatial derivatives are continuous.



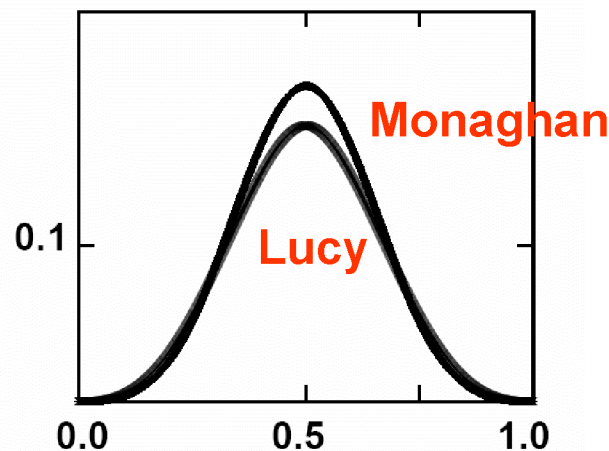
### 3. Spatial Interpolation and Gradients

#### Monaghan and Lucy weight functions in 2 dimensions

$$w_{\text{Lucy}} (r < h) = (5 / 9 \pi h^2) [1 + 3(r / h)] [1 - (r / h)]^3$$

$w$  is normalized and  $w, w', w''$  vanish at  $r = h = 3$ .

$$\rightarrow w_n \propto [1 + n(r / h)] [1 - (r / h)]^n$$



$$w_{\text{Monaghan}} = (40 / 7 \pi h^2) [1 - 6(r / h)^2 + 6(r / h)^3] \quad \text{for } 0 < \frac{r}{h} < \frac{1}{2}$$

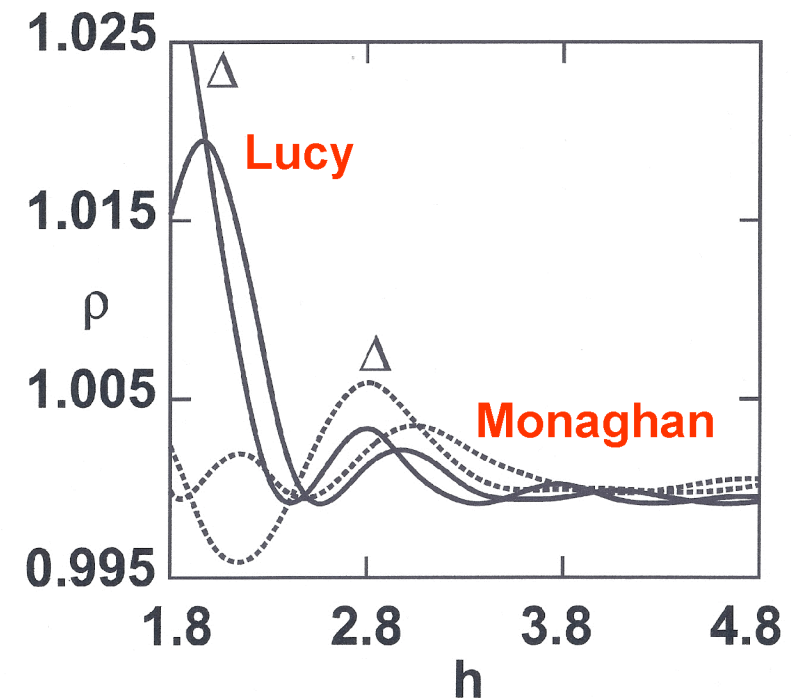
$$w_{\text{Monaghan}} = (80 / 7 \pi h^2) [1 - (r / h)]^3 \quad \text{for } \frac{1}{2} < \frac{r}{h} < 1$$

### 3. Spatial Interpolation and Gradients

Density interpolation converges with ~ 20 neighbors

$$\rho_i = \sum_j w(|\mathbf{r}_i - \mathbf{r}_j|); |\mathbf{r}_i - \mathbf{r}_j| \leq h.$$

- Good estimate for particle smoothing length comes from the summed up densities at regular lattice sites .
- 2D square and triangular lattices with  $h \geq 3$ , lead to errors less than 1% for both weight functions .
- Continuum variables & derivatives (at any point in space) are particle sums .





## 4. Spatial Interpolation and Gradients

### Interpolation for Variables/Gradients Use Particle Sums

- Continuum variables & gradients :

$$\mathbf{r}, \mathbf{v}, \mathbf{e}, P_{xx}, P_{xy}, P_{yy}, Q_x, Q_y, \nabla \mathbf{v}, \nabla T, \nabla \cdot \mathbf{Q}, \nabla \cdot \mathbf{P}.$$

- Use weighted sums of particle variables for interpolation :

$$\rho \mathbf{f}(\mathbf{r}) = \sum_j \mathbf{f}_j w(|\mathbf{r} - \mathbf{r}_j|); \quad \rho_r = \sum_j w(\mathbf{r} - \mathbf{r}_j);$$

$$\nabla(\rho \mathbf{f})_r = \sum_j \mathbf{f}_j \nabla_r w(|\mathbf{r} - \mathbf{r}_j|).$$

- Other powers or functions of density can be used, e. g. ,

$$\mathbf{f}(\mathbf{r}) = \sum_j (\mathbf{f} / \rho)_j w(|\mathbf{r} - \mathbf{r}_j|);$$

$$\mathbf{f}(\mathbf{r}) / \rho = \sum_j (\mathbf{f} / \rho^2)_j w(|\mathbf{r} - \mathbf{r}_j|).$$

#### 4. SPAM versions of the ODEs

Spatial interpolation  $\rightarrow$  Ordinary Differential Equations

$$\dot{\rho}_i = \sum_j (\mathbf{v}_i - \mathbf{v}_j) \cdot \nabla \mathbf{w}_{ij} \quad \text{or} \quad \rho_i = \sum_j \mathbf{w}_{ij} ;$$

$$\dot{\mathbf{v}}_i = - \sum_j [(\mathbf{P} / \rho^2)_i + (\mathbf{P} / \rho^2)_j] \cdot \nabla_i \mathbf{w}_{ij} ;$$

$$\begin{aligned} \dot{\mathbf{e}}_i = & - \sum_j [(\mathbf{P} / \rho^2)_i + (\mathbf{P} / \rho^2)_j] : \frac{1}{2} (\mathbf{v}_i - \mathbf{v}_j) \nabla_i \mathbf{w}_{ij} \\ & - \sum_j [(\mathbf{Q} / \rho^2)_i + (\mathbf{Q} / \rho^2)_j] \cdot \nabla_i \mathbf{w}_{ij} . \end{aligned}$$

Time integration with 4<sup>th</sup> Order Runge-Kutta .

## 5. Runge-Kutta Time Integration (Fourth Order)

$$\dot{\mathbf{r}}_i = \mathbf{v}; \quad \dot{\mathbf{v}}_i = -\sum_j [(\mathbf{P}/\rho^2)_i + (\mathbf{P}/\rho^2)_j] \cdot \nabla_i \mathbf{w}_{ij}.$$

Compute  $\mathbf{r}, \mathbf{v}$  by averaging 4 values of derivatives  $t = \{0, dt/2, dt\}$  :

$$\mathbf{r}(dt) = \mathbf{r}(0) + \frac{dt}{6} (\mathbf{v}_1 + 2\mathbf{v}_2 + 2\mathbf{v}_3 + \mathbf{v}_4);$$

$$\mathbf{v}(dt) = \mathbf{v}(0) + \frac{dt}{6} (\mathbf{a}_1 + 2\mathbf{a}_2 + 2\mathbf{a}_3 + \mathbf{a}_4).$$

---

$$\mathbf{r}_1 = \mathbf{r}(0); \quad \dot{\mathbf{r}}_1 = \mathbf{v}_1 = \mathbf{v}(0); \quad \dot{\mathbf{v}}_1 = \mathbf{a}_1(\mathbf{r}_1);$$

$$\mathbf{r}_2(\frac{dt}{2}) = \mathbf{r}_1 + \frac{dt}{2} \mathbf{v}_1; \quad \mathbf{v}_2(\frac{dt}{2}) = \mathbf{v}_1 + \frac{dt}{2} \mathbf{a}_1; \quad \mathbf{a}_2 = \dot{\mathbf{v}}_2;$$

$$\mathbf{r}_3(\frac{dt}{2}) = \mathbf{r}_1 + \frac{dt}{2} \mathbf{v}_2; \quad \mathbf{v}_3(\frac{dt}{2}) = \mathbf{v}_1 + \frac{dt}{2} \mathbf{a}_2; \quad \mathbf{a}_3 = \dot{\mathbf{v}}_3;$$

$$\mathbf{r}_4(dt) = \mathbf{r}_1 + \mathbf{v}_3 dt; \quad \mathbf{v}_4(dt) = \mathbf{v}_1 + \mathbf{a}_3 dt.$$

## 6. Molecular Dynamics Analogs Trajectory Isomorphisms

- Two interesting cases of trajectory isomorphisms occur with SPAM and molecular dynamics .

**Lucy fluid** For  $P = \rho^2 / 2$  trajectories are the same if  $w_{ij} \text{ spam} \rightarrow \Phi_{ij} \text{ md}$  .

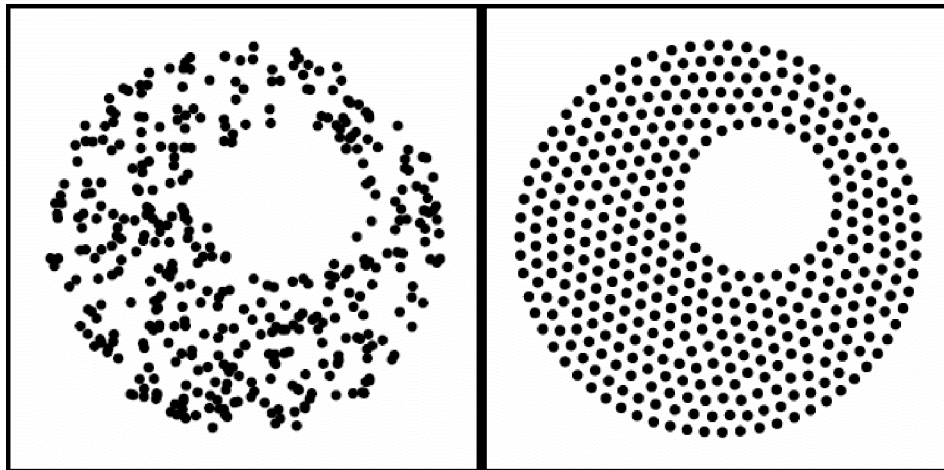
**Embedded-atom fluid** For  $P = \rho^3 - \rho_0 \rho^2$  trajectories are the same if 
$$\Phi = \sum_j \frac{1}{2} \left( \frac{\rho_j}{\rho_0} - 1 \right)^2 .$$

- Lucy fluid is used for the free expansion problem .
- Embedded atom can be used for structural relaxation and the collapsing water column .

## 7. Mesh Generation & Boundary Conditions

### Meshes for Irregular Shapes and Lattices

- Use viscous relaxation techniques from molecular dynamics .

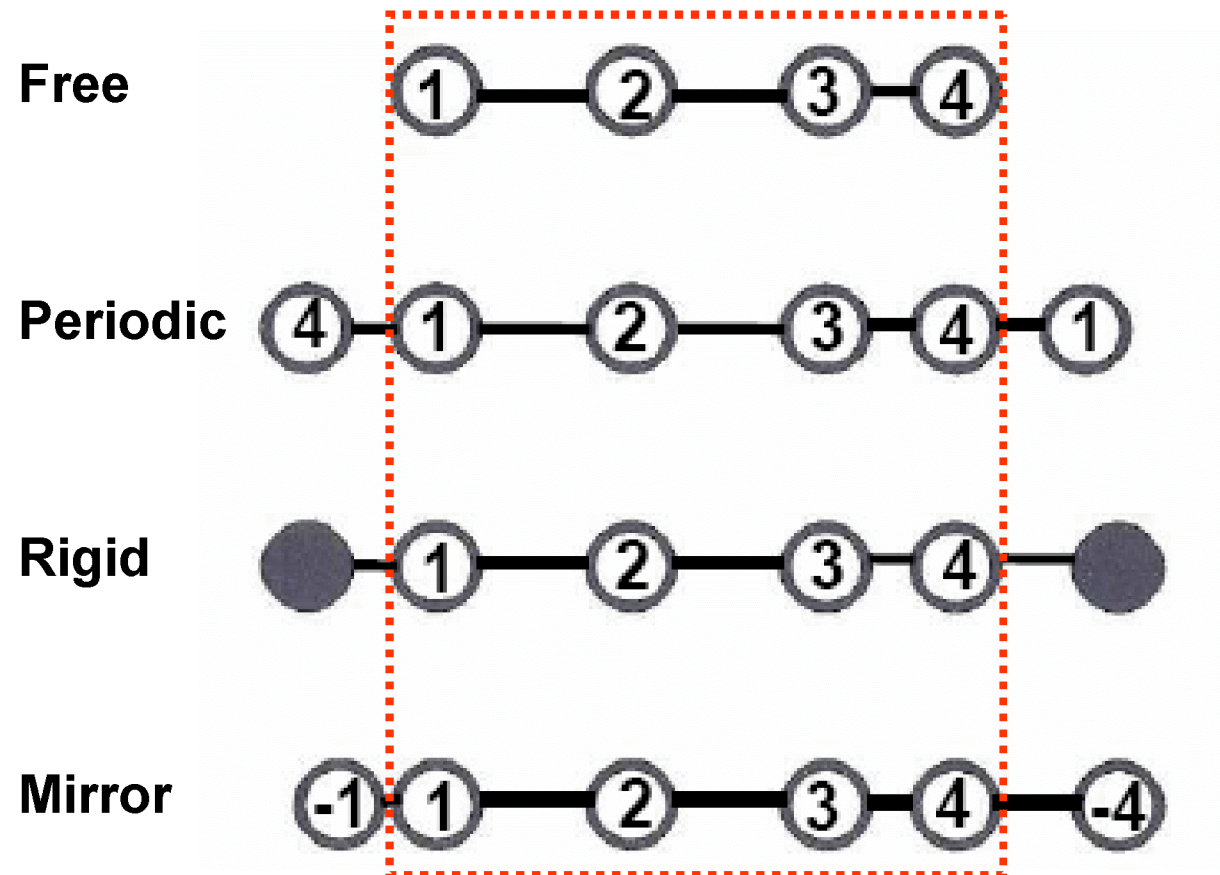


- Test lattice structures for stability → Use density curvature potential .
- Select surface treatment using surface tension or  $\sum_j (\nabla \rho)^2$  potential .



## 7. Mesh Generation & Boundary Conditions

### Free, Periodic, Rigid & Mirror Boundaries



## 8. Maladies and Cures

### Lattices with $e(\rho)$ are typically unstable!

Two-dimensional MD lattices with the usual pair potentials are stable .

SPAM/MD lattices with the following density-dependent internal/potential energy are typically NOT stable for any simple two dimensional lattice .

$$e_j \equiv \frac{1}{2} (\rho_j - \rho_0)^2 \longrightarrow \mathbf{P} = \rho^2 (\partial \mathbf{e} / \partial \rho) = \rho^2 (\rho - \rho_0)$$

$$\Phi_\rho \equiv \sum_j (\rho_j - \rho_0)^2 ; \rho = \sum_j w_{ij}$$

These lattices do not have any shear resistance and melt :

Particle sum estimates are misleading:  $G \approx \nabla^2 e(\rho) \approx \frac{90}{7\pi h^4} \neq 0$  ;

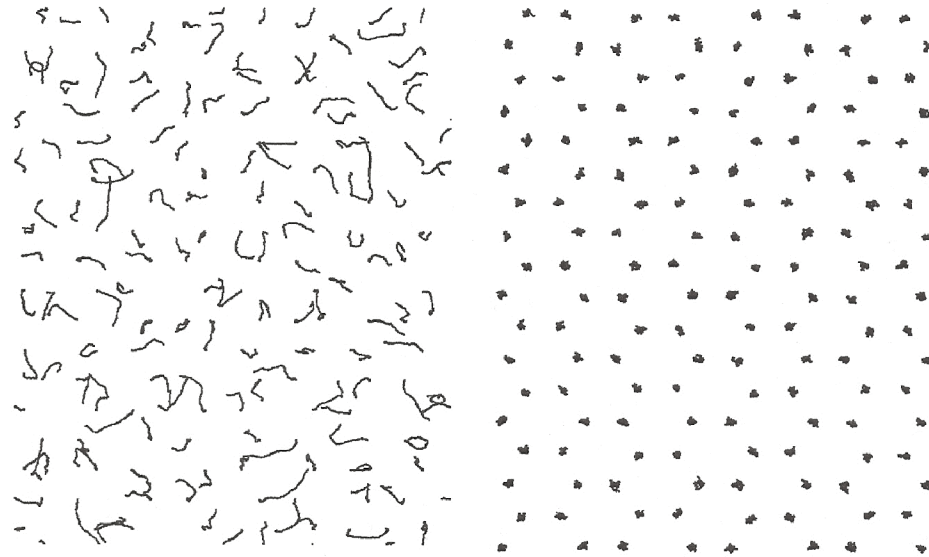
Evaluation of the elastic constants :  $G = C_{44} = 0$  !

Hoover *et ux*, Physical Review E 73, 01672 (2006) .

Density-gradient potentials provide surface tension. An invariant curvature potential provides elastic shear strength,  $G > 0$  .

## 8. Maladies and Cures

### Invariant Curvature Potential Cures Lattice Instability



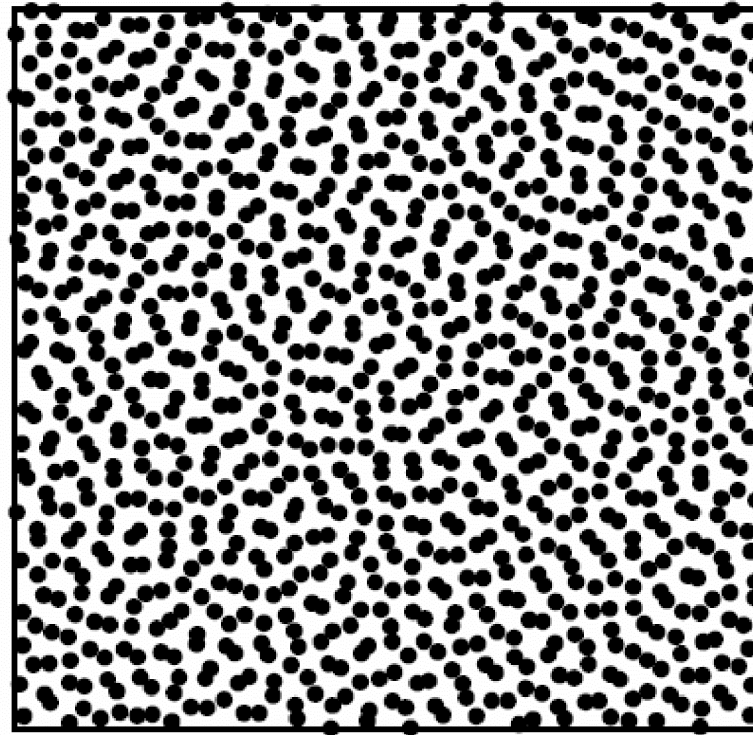
Particle trajectories in a two-dimensional hexagonal lattice. Initial particle displacements were chosen randomly with zero sum. Lattice is unstable (left) and is stabilized (right) by adding the invariant curvature potential .

$$\Phi = (\rho_{xx} - \rho_{yy})^2 + 4(\rho_{xy})^2 ;$$

$$\rho_{xx} = \partial^2 \rho / \partial x^2 , \rho_{yy} = \partial^2 \rho / \partial y^2 , \rho_{xy} = \partial^2 \rho / \partial x \partial y .$$

## **8. Maladies and Cures**

### **String Phases Are Cured with Core Potentials**

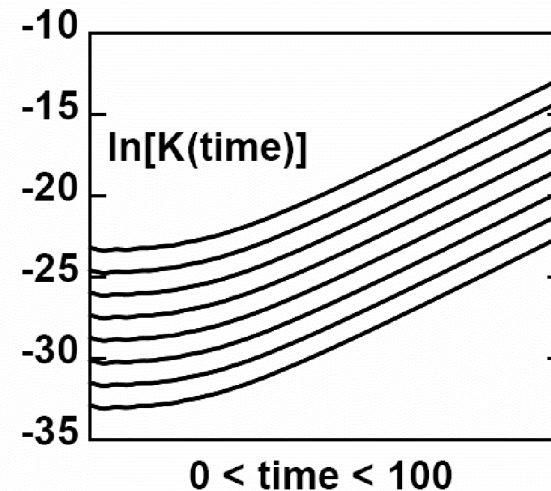


**A relaxed periodic structure with an embedded atom equation of state, using Lucy's weight function with  $h = 3.5$  . The cure for the string formation is to add a core potential so that particles cannot get too close .**

## 8. Maladies and Cures Tensile Instability

- Kinetic energy growth in an isotropic solid under uniform tension .

The kinetic energy of a single particle moving slowly ( $\sim 10^{-8}$  or smaller) will increase exponentially at a time longer than the inverse Einstein frequency .



- Three useful cures :

1. Add von Neumann-Richtmyer artificial viscosity ;
2. Introduce a repulsive core potential ;
3. Modify the relationship between  $r$  and  $v$  (Monaghan) :

$$\dot{\mathbf{r}} = \mathbf{v} \rightarrow \dot{\mathbf{r}} = \mathbf{v}_i + \sum_j (\mathbf{v}_j - \mathbf{v}_i) \frac{w_{ij}}{\rho_{ij}} ;$$

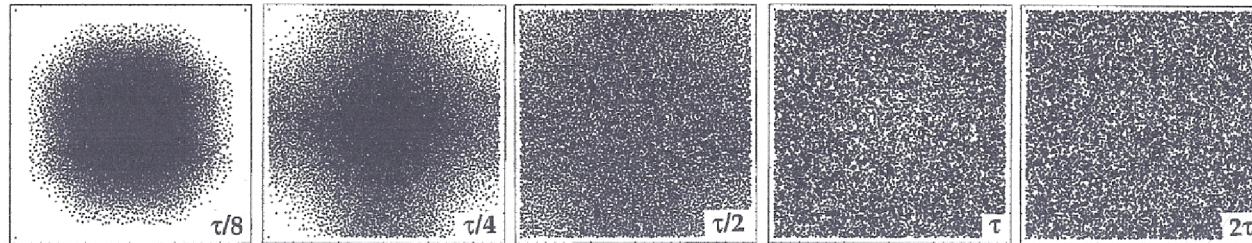
$$\rho_{ij} = \sqrt{\rho_i \rho_j} \text{ or } \rho_{ij} = \frac{1}{2}(\rho_i + \rho_j) .$$



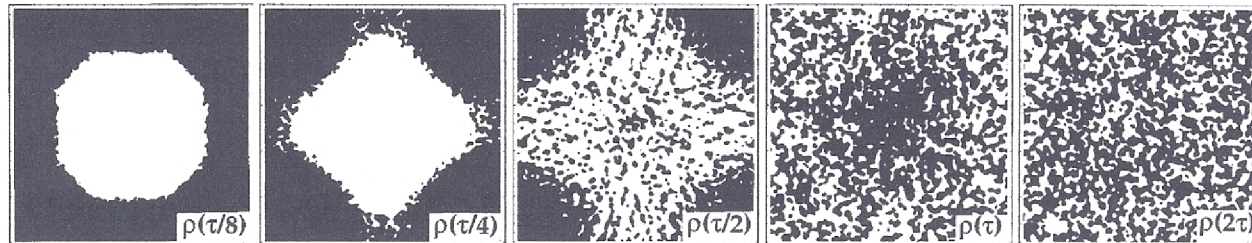
## 9. SPAM Results: Free Expansion of 16,384 particles:

$\tau$  is the time relative to the sound traversal time . Light regions are above the average and dark regions are below the average .

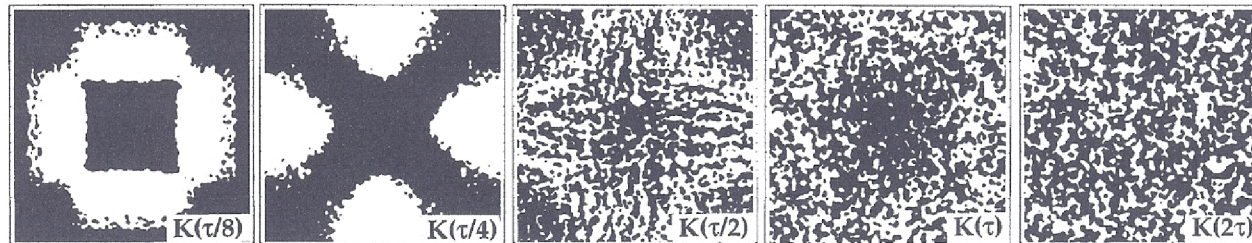
Particle motion



Density



Kinetic energy



$$V_0 = 1/4V_f, \text{ Lucy fluid with } h = 6.$$

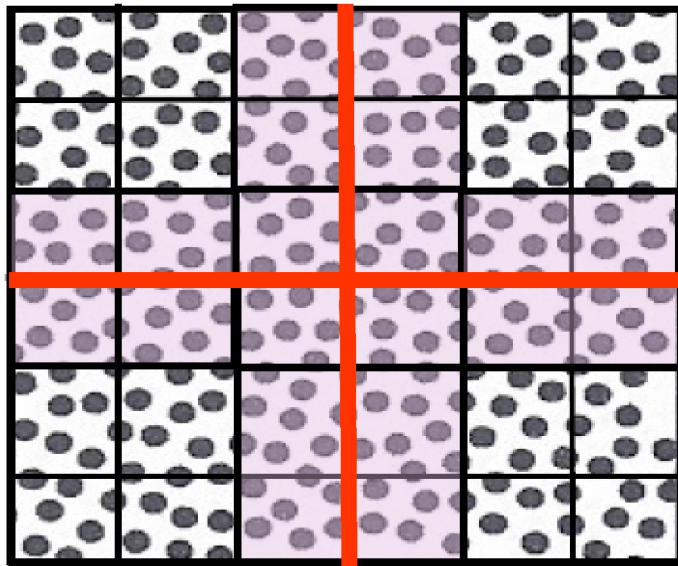
Hoover, Posch, Physical Review E 59, 1770-1776 (1999) .

Hoover, Posch, Castillo, *et ux*, Journal of Statistical Physics, 100, Nos. 1/2, (2000) .

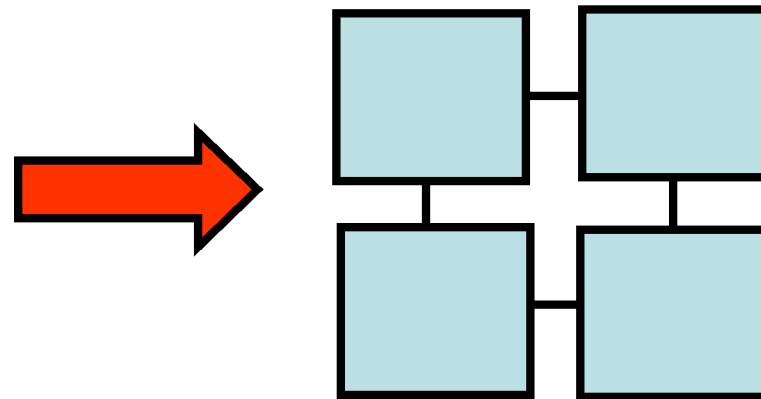
## 10. Parallel Techniques for Fluids and Solids Eulerian Grid of Particle-Cells → Processors

- Two forms of parallel are “shared memory” and “message-passing” .
- Must use message-passing for large problems .
- Message-passing is more **efficient**, works for **larger problems**, but is **much more difficult** to program .

Message-passing technique



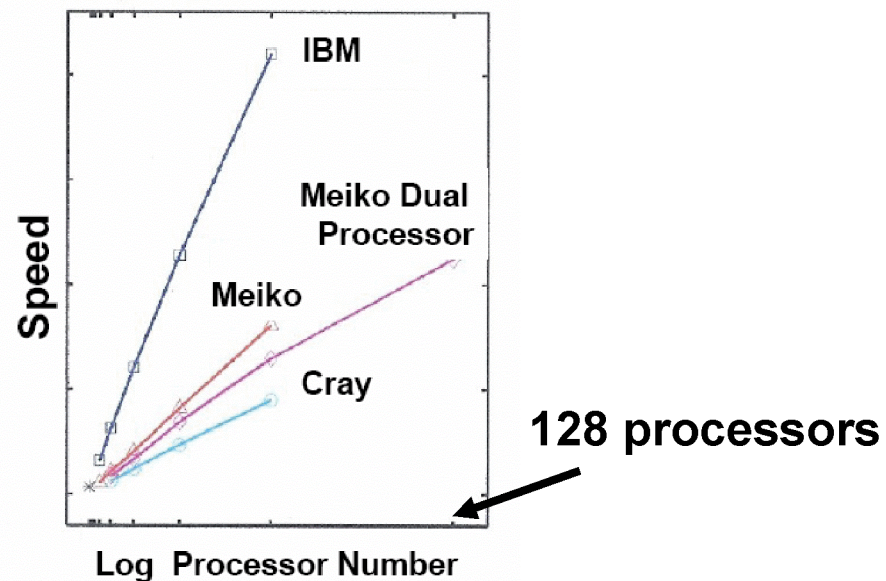
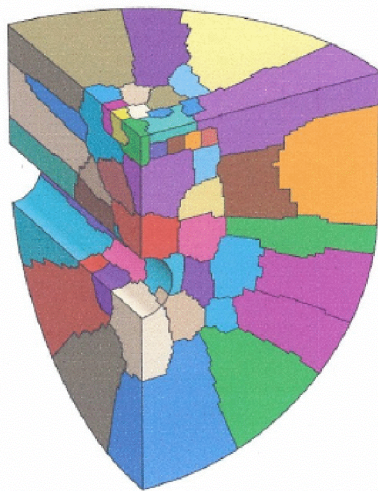
Four-processor parallel computer



## 10. Parallel Techniques Efficiency, Scalability & Message-Passing

- Communication time reduces parallel efficiency

$$S = \tau_1 / \tau_N = N\eta \leq N = N\eta_{\text{ideal}}$$



- Message-passing involves detailed lists tracking cells/particles in processors .

## 10. Parallel Techniques

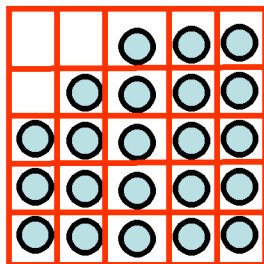
### Create Subdomains from Optimized Cuts of Graphs

- **Goal:** Domain split into subdomains . Subdomain  $\rightarrow$  processor .
- **Method:** Convert domain  $\rightarrow$  weighted graph :  
cells  $\Rightarrow$  vertices  
cell connectivity  $\Rightarrow$  lines
- Optimized cuts of graphs are *partitions* (subdomains) .

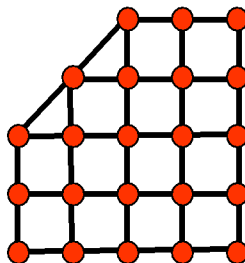
Method by Karypis and Kumar + free software :

<http://www.cs.umn.edu/~metis/>

Particles  
in  $dx \sim h$



Graph with  
connected cells



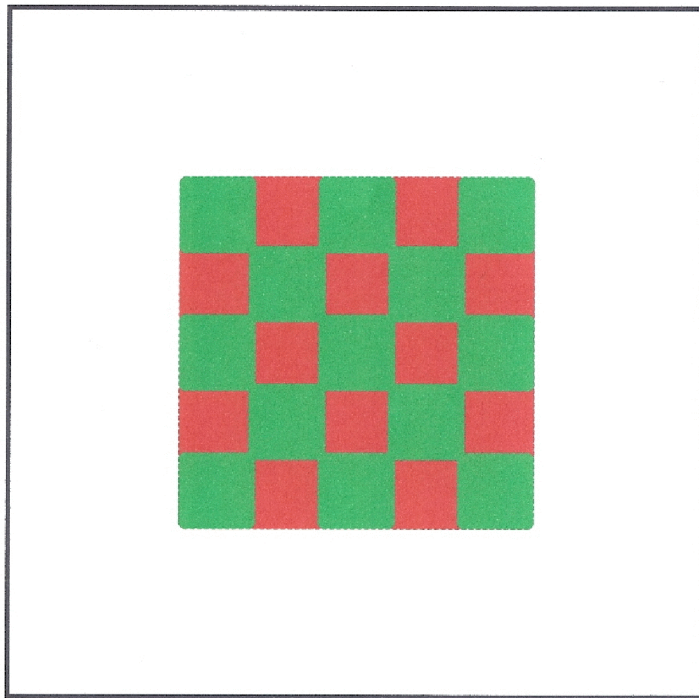
Vertex weights  $\propto$  processor work time  
Line weights  $\propto$  communication time



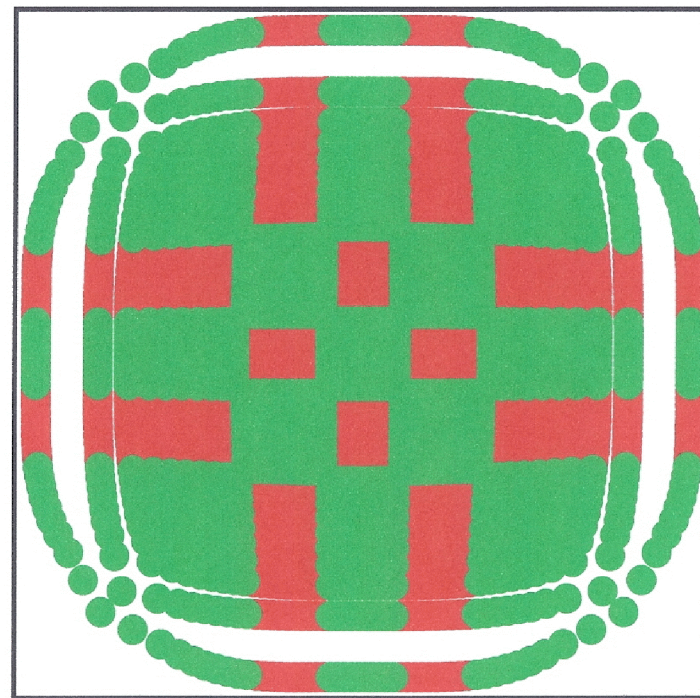
## 10. Parallel Techniques

### Example: Dynamically Partitioned Free Expansion

Repartition at any time during the calculation when there is a load imbalance .



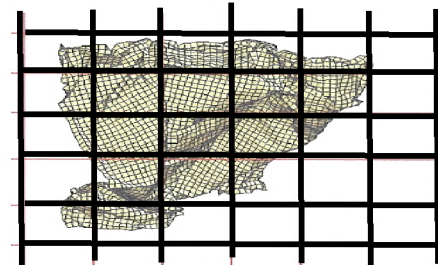
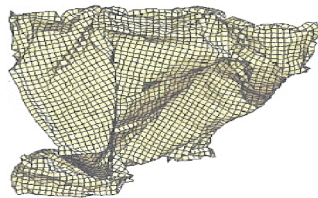
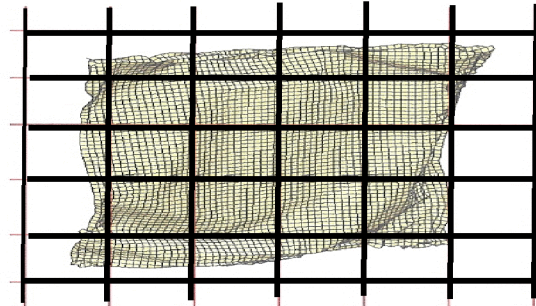
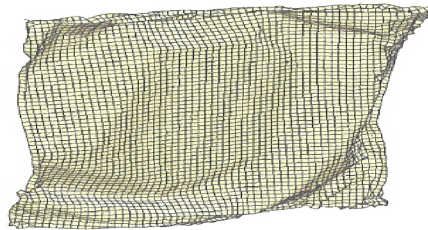
$$-25 < (x, y) < +25$$



$$-25 < (x, y) < +25$$

## 10. Parallel Techniques

Example: **Dynamically Partitioning** Crushed Sheet



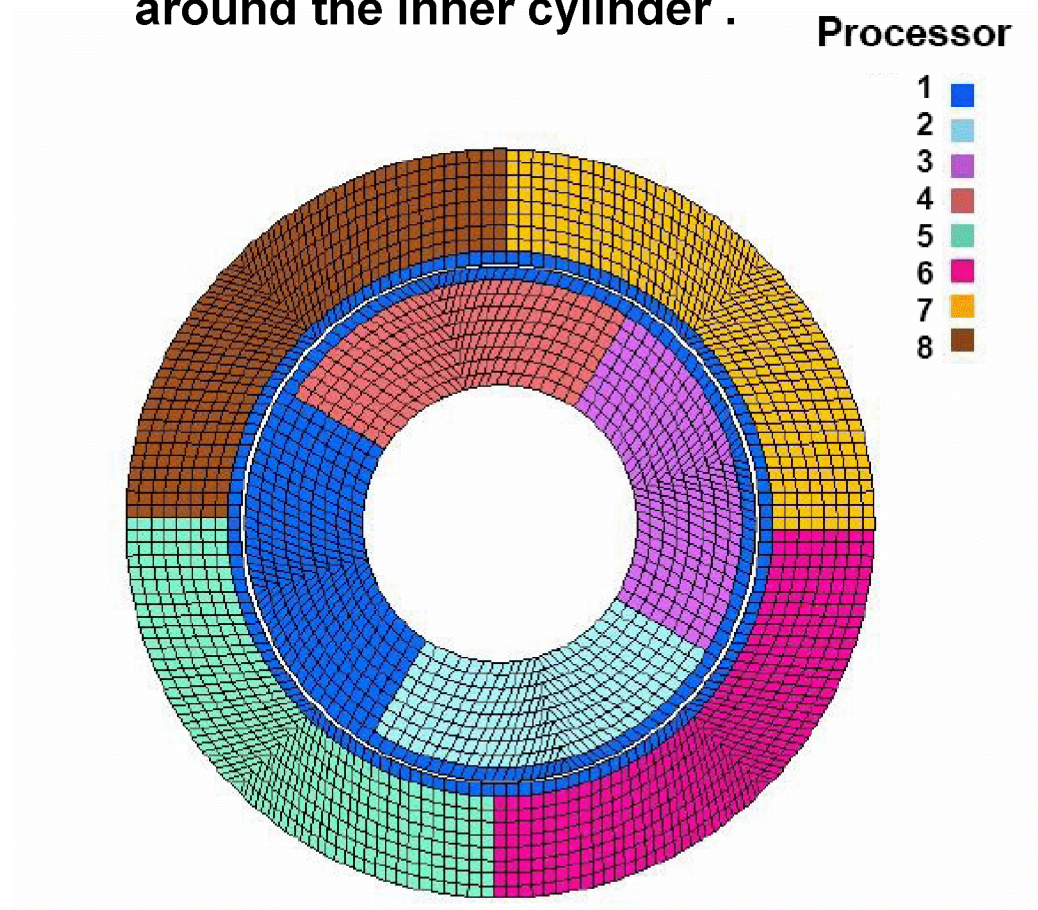
**This complex surface folding leads to arbitrary “self contact” .  
This is a hard problem on single processor computers !!**

## 10. Parallel Techniques

### Example: Partitioned “Nut-Bolt” Mesh and Interface

- Treat the surfaces as a separate partition ;
- For many surfaces, distribute them among several processors .
- Surface partition is computed only once for this problem .

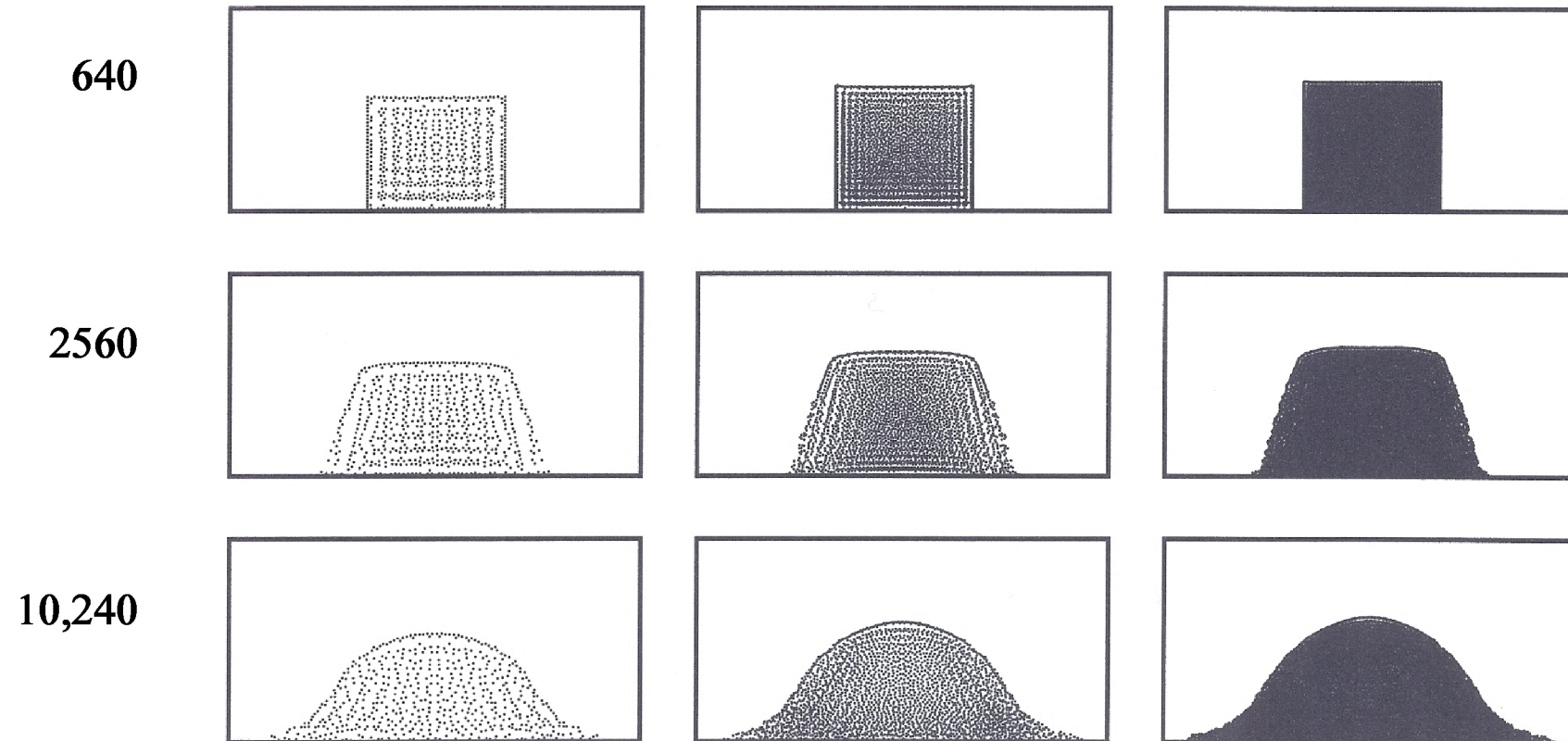
The outer cylinder rotates around the inner cylinder .





# 11. Collapsing water column with gravity

**N = 640, 2560, 10,240 particles**

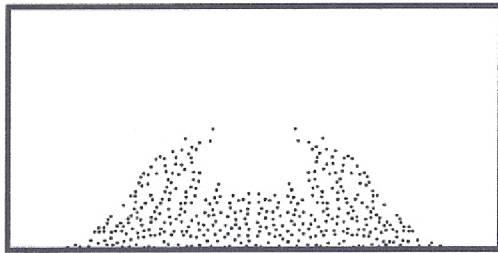


$$t_{10240} = 2t_{2560} = 4t_{640}$$

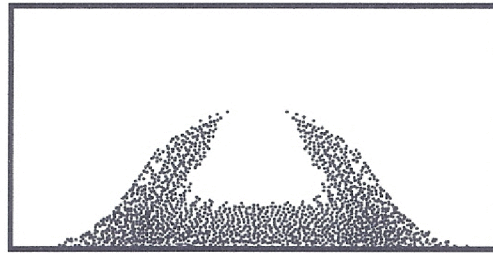
Uses  $\Phi_{EA}$ ,  $\Phi_{\text{surface}} \propto \sum_j (\nabla \rho)_j^2$ ,  $\Phi_{\text{core}}$ .

# 11.Collapsing water column with gravity

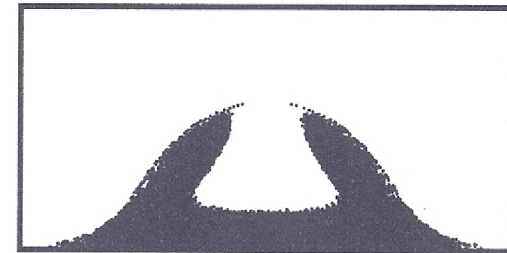
## Tensile regions – SPAM and Finite Elements



640 particles



2560 particles

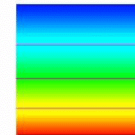


10,240 particles

WxH = 80x64 elements  
 $dy = 2dx = 1$



$g = 0$



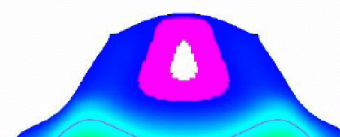
$t = 0$

Relaxation

Cavitation model :  
 $P > P_c \rightarrow P = P_c$



$t = 30$

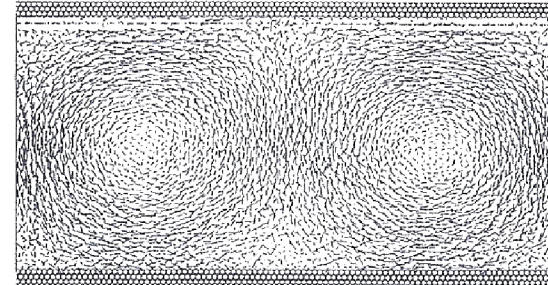
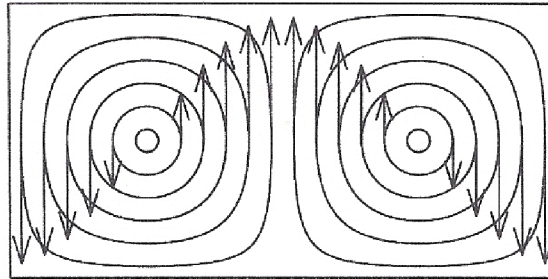


$t = 40$

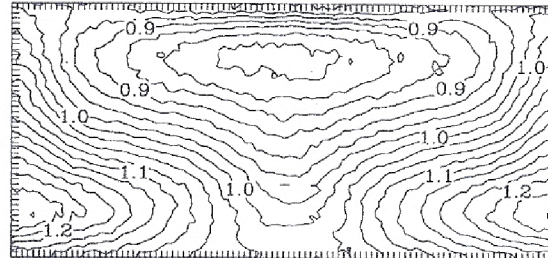
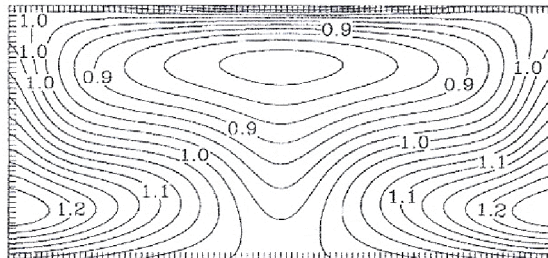
Collapse

## 12. Rayleigh-Bénard Flow (Gravity & T gradient) Finite-Difference (left) & Smooth Particles (right)

Velocity

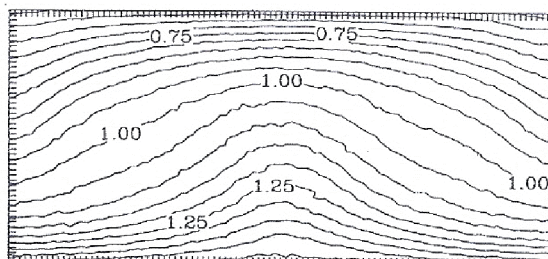
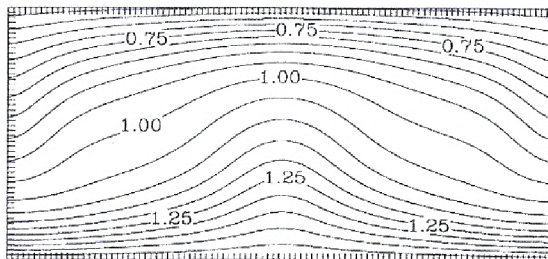


Density



Gravity  
↓

Temperature



**T = 0.5**

**T = 1.5**

Rolls form for  $R_c = \frac{gL^4(d\ln T/dy)}{\nu D_T}$  & 5000 smooth particles

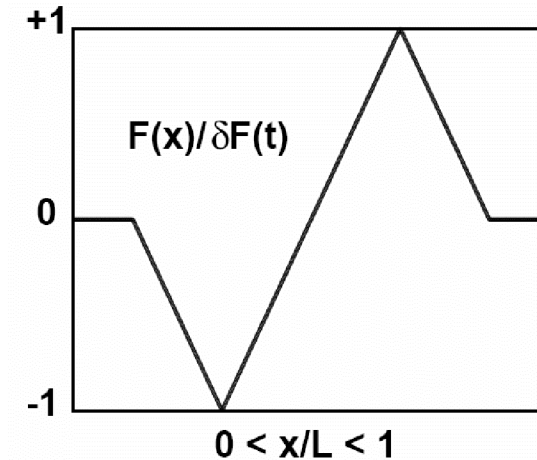
Kum, Hoover, & Posch, PRE 52, 4899-4908 (1995) .



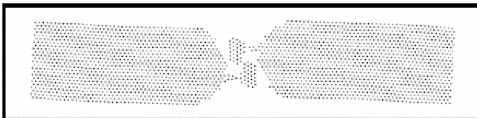
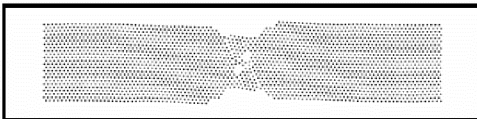
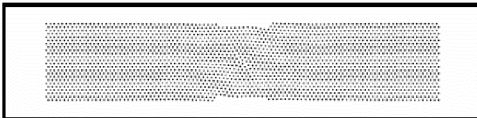
# 13. a) Tension Test with Particles

## Pair $\Phi$ MD, core $\Phi$ , density-gradient $\Phi$ & strength

- External forces applied to the interior of a tension specimen ;
- Initially tapered bar .

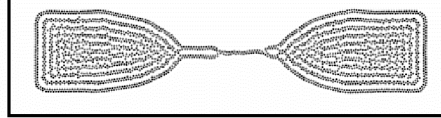
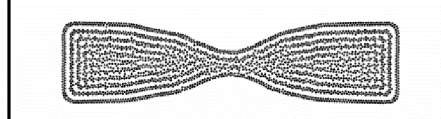
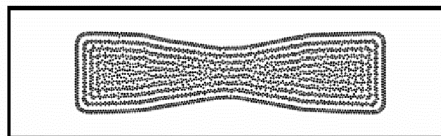


- Three tension-test particle simulations :



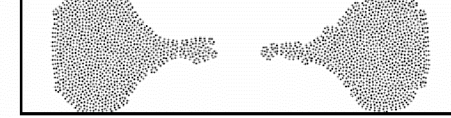
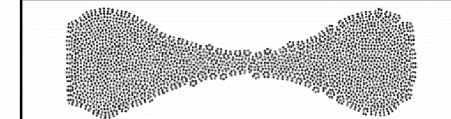
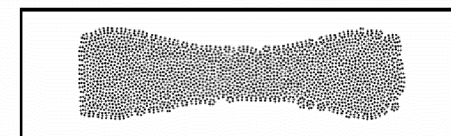
$-60 < x < +60$  ;  $t = 620, 624, 628$

Pair-potential MD



$-70 < x < +70$  ;  $t = 375, 625, 875$

SPAM + core potential



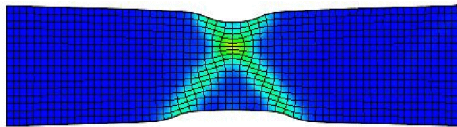
$-70 < x < +70$  ;  $t = 10000, 15000, 20000$

SPAM-like MD:  
core +  $\sum_j (\nabla \rho)^2$  + strength

## 13 a) Tension Test with DYNA3D

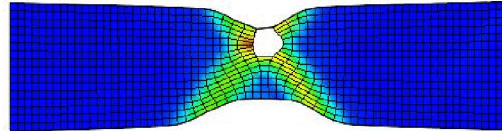
### Finite-Element Simulation of Tension Test

A tapered bar is created with elements reduced in height by 10% from the end of the bar to the middle of the bar. A time dependent load is applied to the ends of the bar.



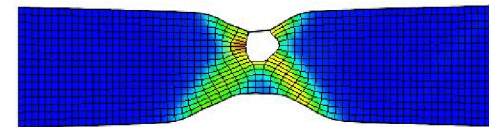
**Time = 32**

$$\varepsilon_p = .05$$



**Time = 48**

$$\varepsilon_p = .075$$

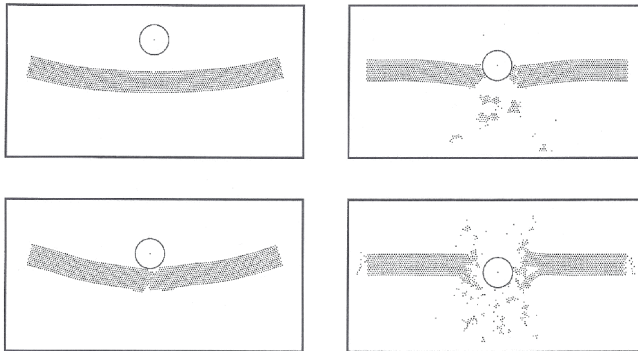


**Time = 64**

$$\varepsilon_p = .100$$

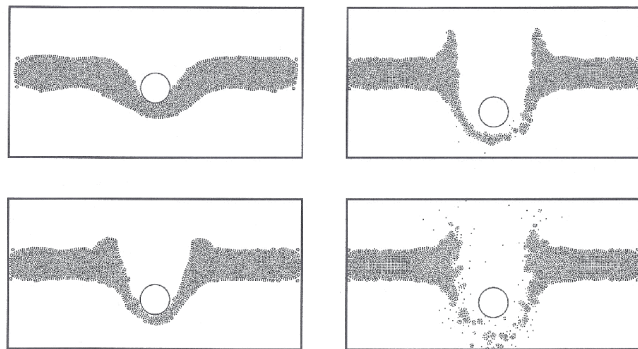
**Plastic flow begins at  $\varepsilon = \delta L/L = .01$**

## 13 b) Ball-Plate Fragmentation Ball-Plate Penetration with Particles



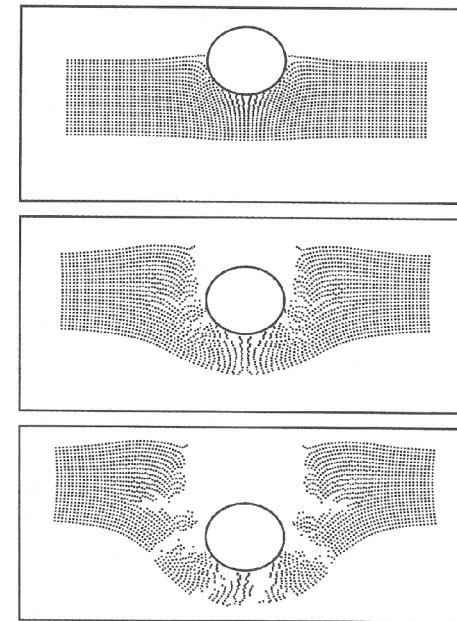
$-70 < x < +70$  ;  $v = 1, 2, 4, 8$

**Pair potential MD**



$-100 < x < +100$  ;  $v = 1/4, 1/2, 1, 2$

**MD + embedded-atom & strength**

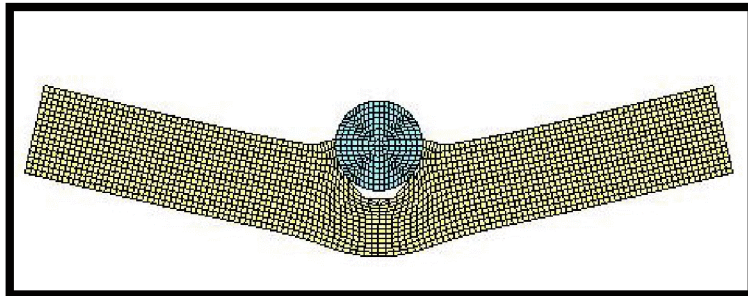


$-60 < x < +60$  ;  $t = 4, 12, 20$

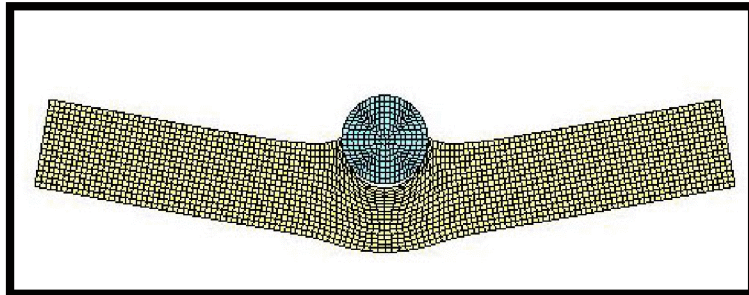
**SPAM**

## 13 b) Ball-Plate Fragmentation Ball-plate Penetration with Finite Elements

$$V_0 = 1/4 ; \epsilon_f = (1.0, 2.0)$$

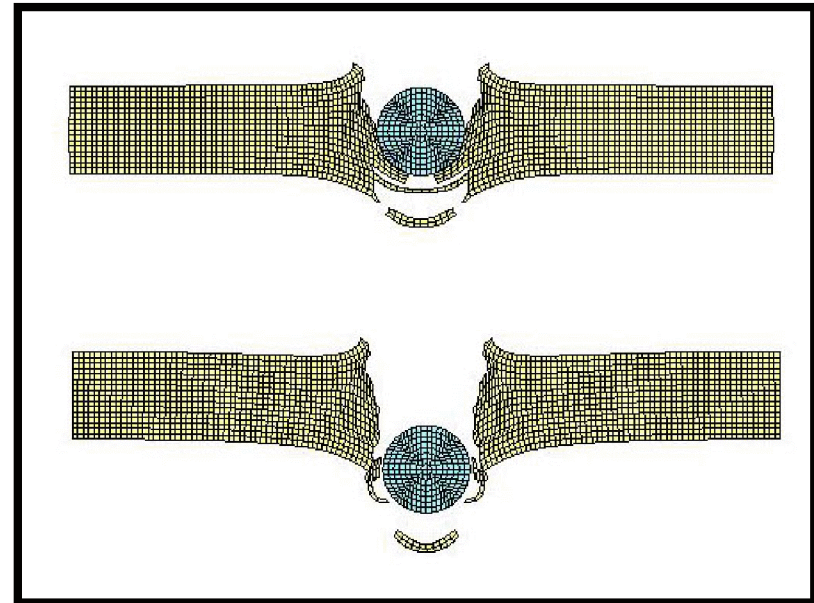


$$\epsilon_p < \epsilon_f = 1.0, v_0 = 1/4$$



$$\epsilon_p < \epsilon_f = 2.0, v_0 = 1/4$$

$$V_0 = 1/2 ; \epsilon_f = 1.0$$



$$\epsilon_p < \epsilon_f = 1.0, v_0 = 1/2$$

For the lower velocity (left) the ball bounces back, but leaves a permanent deformation . For the higher velocity the ball breaks through the plate .



## **Conclusion – SPAM Is a Transparent, Pedagogical Particle Method for Simulating Continuum Dynamics**

### **➤ SPAM is useful for modeling continuum mechanics**

**Algorithm is transparent to program & easier to debug ;  
Algorithm avoids mesh tangling that stops mesh-based calculations ;  
Rezoning is easy .**

### **➤ Various deficiencies have been cured**

**Density-gradient potential for lattice surfaces ;  
String phases cured with core potentials ;  
Density-curvature potential for strength .**